

## **Downstream Impact Analysis**

## for

## **Mack Todd Road Townhomes**

Zebulon North Carolina



**Prepared by:** 

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## **Project Narrative**

The proposed residential project is located on a 2.3 acre vacant, mostly wooded lot. The proposed development includes construction of 13 townhomes. The site is located in Zebulon, NC, and is located in the Neuse River watershed basin .

### **Downstream Impact Analysis**

#### **Requirements:**

Per Zebulon ordinance 151.36, the following is required:

(A) Downstream impact analysis.

(1) The downstream impact analysis must be performed in accordance with the "10% rule," and a copy of the analysis must be provided with the permit application. The purpose of the downstream impact analysis is to determine if the project will cause any impacts on flooding or channel degradation downstream of the project site. The analysis must include the assumptions, results and supporting calculations to show safe passage of post-development design flows downstream. This analysis shall be performed at the outlet(s) of the site, and downstream at each tributary junction to the point(s) in the conveyance system where the area of the portion of the site draining into the system is less than or equal to 10% of the total drainage area above that point.

(2) The typical steps in the application of the 10% rule are:

(a) Using a topographic map, determine the point downstream where the proposed site equals 10% of the total drainage area, called the 10% point. Identify all tributary junctions between the downstream site boundary and the 10% point. All points identified, as well as the outlet of the site, are known as 10% rule comparison points.

(b) Using a hydrologic model with existing land uses, determine the pre-development peak runoff rate (cfs) for the ten-year design storm event at each comparison point.

(c) Insert the proposed site design and proposed BMPs into the land uses and determine the post-development peak runoff rate for the ten-year design storm at each comparison point.

(d) If the post-development peak discharge rate is equal to or less than pre-development conditions at all comparison points, no further analysis is required

#### Methodolgy:

The site is adjacent to an existing stream. All runoff from the project discharges into this stream at the SE corner of the property. The drainage area at this point is 307 acres. The project site is 2.3 acres. Therefore, a point directly off-site of the property is the point at which the site is 10% of the total drainage area. This is the downstream analysis point . There are no tributary junctions between the downstream site boundary and the downstream analysis point.

#### **Drainage Area calculations:**

<u>Pre-developed</u> Drainage Area = 307 acres Assume C soils and CN=70 Q10 = 686 cfs

#### Post-developed

The total post-developed flow at the analysis point was obtained by combining the routed postdeveloped hydrograph, the post-developed bypass hydrograph, and the pre-developed hydrograph to get a total post-developed flow at the discharge point. Q10 = 687 cfs.

Please refer to the Stormwater Management Report for complete calculations for the SCM routing and bypass hydrographs.

#### **Conclusion**

The pre and post-development flows are essentially unchanged (0.15% increase), and there are no points to analyze, therefore, no further analysis is required.





#### Legend

#### Hyd. Origin Description

1	SCS Runoff	DP #1 - PRE
2	SCS Runoff	DP#1 - POST TO SCM

- 3 SCS Runoff DP #1 BYPASS
- 4 Reservoir Routing
- 5 Combine Total flow at Discharge point #1

Project: F:\Projects\CPMTRZ\Storm\DIA\dia - CPMTRZ-hydrographs.gpw

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#### Hyd. No. 1

DP #1 - PRE

Hydrograph type	= SCS Runoff	Peak discharge	= 685.52 cfs
Storm frequency	= 10 yrs	Time to peak	= 12.17 hrs
Time interval	= 2 min	Hyd. volume	= 2,568,477 cuft
Drainage area	= 320.000 ac	Curve number	= 70*
Basin Slope	= 2.0 %	Hydraulic length	= 5000 ft
Tc method	= KIRPICH	Time of conc. (Tc)	= 24.80 min
Total precip.	= 5.28 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

\* Composite (Area/CN) = [(1.200 x 70) + (0.400 x 74)] / 320.000



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### Hyd. No. 2

DP#1 - POST TO SCM

Hydrograph type =	SCS Runoff	Peak discharge	= 6.550 cfs
Storm frequency =	= 10 yrs	Time to peak	= 11.93 hrs
Time interval =	= 2 min	Hyd. volume	= 14,112 cuft
Drainage area =	= 1.000 ac	Curve number	= 90*
Basin Slope =	= 0.0 %	Hydraulic length	= 0 ft
Tc method =	= User	Time of conc. (Tc)	= 5.00 min
Total precip. =	= 5.28 in	Distribution	= Type II
Storm duration =	= 24 hrs	Shape factor	= 484

\* Composite (Area/CN) = [(0.680 x 98) + (0.320 x 74)] / 1.000



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### Hyd. No. 3

DP #1 - BYPASS

Hydrograph type	= SCS Runoff	Peak discharge	= 3.797 cfs
Storm frequency	= 10 yrs	Time to peak	= 11.97 hrs
Time interval	= 2 min	Hyd. volume	= 7,645 cuft
Drainage area	= 0.930 ac	Curve number	= 72*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 5.00 min
Total precip.	= 5.28 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

\* Composite (Area/CN) = [(0.460 x 70) + (0.470 x 74)] / 0.930



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### Hyd. No. 4

Routing

Hydrograph type	= Reservoir	Peak discharge	= 6.366 cfs
Storm frequency	= 10 yrs	Time to peak	= 11.97 hrs
Time interval	= 2 min	Hyd. volume	= 14,014 cuft
Inflow hyd. No.	= 2 - DP#1 - POST TO SCM	Max. Elevation	= 281.09 ft
Reservoir name	= SCM	Max. Storage	= 4,104 cuft

Storage Indication method used.



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### Hyd. No. 5

Total flow at Discharge point #1

$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Hydrograph type	= Combine	Peak discharge	= 687.05 cfs
	Storm frequency	= 10 yrs	Time to peak	= 12.17 hrs
	Time interval	= 2 min	Hyd. volume	= 2,590,134 cuft
	Inflow hyds.	= 1, 3, 4	Contrib. drain. area	= 320.930 ac

